

RARITAN RIVER BASIN STONY BROOK TRIBUTARY MERCER COUNTY

NEW JERSEY

LEVEE

STONY BROOK DAM NO.3 NJ 00389

PHASE 1 INSPECTION REPORT

BNATIONAL DAM SAFETY PROGRAM.

Stony Brook Dam, Number 3 (NJ00389).
Raritan River Basin, Stony Brook Tributary,
Mercer County, New Jersey. Phase 1 Inspection
Report.

COPY

Final Rept. // F. Keith /Jolls



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DEPARTMENT OF TH

Philadelphia District Corps of Engineers

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19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

Spillway . Dams

National Dam Inspection Report

Safety

Structural Analysis Visual Inspection

Stony Brook Dam No. 3, N.J.

20. ABSTRACT (Continue on reverse side if necessary and identity by block number)

This report cites results of a technical investigation as to the dam's adequacy. The inspection and evaluation of the dam is as prescribed by the National Dam Inspection Act, Public Law 92-367. The technical investigation includes visual inspection, review of available design and construction records, and preliminary structural and hydraulic and hydrologic calculations, as applicable. An assessment of the dam's general condition is included in the report.

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SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)

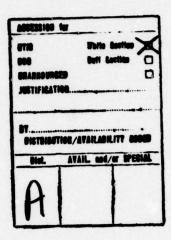
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DEPARTMENT OF THE ARMY PHILADELPHIA DISTRICT, CORPS OF ENGINEERS CUSTOM HOUSE-2D & CHESTNUT STREETS PHILADELPHIA, PENNSYLVANIA 19106

Honorable Brendan T. Byrne Governor of New Jersey Trenton, New Jersey 08621



7 MAY 1979

Dear Governor Byrne:

Inclosed is the Phase I Inspection Report for Stony Brook Dam No. 3 in Mercer County, New Jersey which has been prepared under authorization of the Dam Inspection Act, Public Law 92-367. A brief assessment of the dam's condition is given in the front of the report.

Based on visual inspection, available records, calculations and past operational performance, Stony Brook Dam No. 3, initially listed as a high hazard potential structure but reduced to a low hazard potential structure as a result of this inspection, is judged to be in good overall condition and the spillway is considered adequate. The low hazard potential classification means that in the event of failure of the dam, no loss of life and only minimal economic loss is expected. The following remedial actions could be undertaken by the owner:

- (1) Regrade the eroded backslopes and sides and reseed the barren areas.
- (2) Continue monitoring the backslope seepage and the subgrade drains.
- (3) Consider providing additional training for park personnel relative to maintenance and inspection.

A copy of the report is being furnished to Mr. Dirk C. Hofman, New Jersey Department of Environmental Protection, the designated State Office contact for this program. Within five days of the date of this letter, a copy will also be sent to Congressman James A. Courter of the Thirteenth District. Under the provisions of the Freedom of Information Act, the inspection report will be subject to release by this office, upon request, five days after the date of this letter.

NAPEN-D Honorable Brenden T. Byrne

Additional copies of this report may be obtained from the National Technical Information Services (NTIS), Springfield, Virginia 22161 at a reasonable cost. Please allow four to six weeks from the date of this letter for NTIS to have copies of the report available.

An important aspect of the Dam Safety Program will be the implementation of the recommendations made as a result of the inspection. We accordingly request that we be advised of proposed actions taken by the State to implement our recommendations.

Sincerely,

1 Incl As stated JAMES G. TON Colonel, Corps of Engineers District Engineer

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Copies furnished:
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STONY BROOK DAM NO. 3 (NJ00389)

CORPS OF ENGINEERS ASSESSMENT OF GENERAL CONDITIONS

This dam was inspected on 8 December 1978 by Louis Berger and Associates, Inc. under contract to the State of New Jersey. The State, under agreement with the U. S. Army Engineer District, Philadelphia, had this inspection performed in accordance with the National Dam Inspection Act, Public Law 92-367.

Stony Brook Dam No. 3, initially listed as a high hazard potential structure but reduced to a low hazard potential structure as a result of this inspection, is judged to be in good overall condition and the spillway is considered adequate. The low hazard potential classification means that in the event of failure of the dam, no loss of life and only minimal economic loss is expected. The following remedial actions could be undertaken by the owner:

- (1) Regrade the eroded backslopes and sides and reseed the barren areas.
- (2) Continue monitoring the backslope seepage and the subgrade drains.

(3) Consider providing additional training for park personnel relative to maintenance and inspection.

APPROVED Times

JAMES G. TON

Colonel, Corps of Engineers

District Engineer

DATE: 11/12/1979

PHASE I REPORT NATIONAL DAM INSPECTION PROGRAM

Name of Dam Stony Brook Dam No. 3 Fed ID# NJ 00389 NJ ID# 584

State Located New	Jersey
County Located Me	rcer
	4019.9 - Long. 7445.4
	(unnamed) to Stony Brook
Date of Inspection	8 December 1978

ASSESSMENT OF GENERAL CONDITIONS

Stony Brook Dam No. 3 is in a good overall condition and has an adequate spillway capacity to accommodate the 100-year design flood. It is recommended that its hazard classification be downgraded to low as its overtopping or collapse would not increase the danger of loss of life or property damage. No detrimental findings were uncovered to merit further study. Recommended remedial actions to be undertaken in the future as part of the County Parks maintenance program include repair and seeding of the eroded areas of all slopes and the additional training of operating personnel relative to dam maintenance and inspection.

F. Keith Joll

Project Manager



OVERVIEW OF STONY BROOK WATERSHED DAM SITE #3

DECEMBER, 1978

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PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The test flood provides a measure of relative spillway capacity and serves as an aide in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM NAME OF DAM: STONY BROOK NO. 3 FED# NJ 00389

SECTION 1 - PROJECT INFORMATION

1.1 GENERAL

a. Authority

This report is authorized by the Dam Inspection Act, Public Law 92-367, and has been prepared in accordance with contract FPM-36 between Louis Berger & Associates, Inc. and the State of New Jersey and its Department of Environmental Protection, Division of Water Resources. The State in turn, is under agreement with the U.S. Army Engineer District, Philadelphia, to have this inspection performed.

b. Purpose of Inspection

The purpose of this inspection is to evaluate the structural and hydraulic condition of the Stony Brook Watershed No. 3 and appurtenant structures, and to determine if the dam constitutes a hazard to human life or property.

1.2 DESCRIPTION OF PROJECT

a. Description of Dam and Appurtenances

The dam at Stony Brook Watershed Site No. 3 (a.k.a. Johnstons Lake) is a two zone, 1,900 foot long, curvilinear earth structure with an impermeable core and cutoff key. The principal discharge outlet consists of a reinforced concrete drop inlet with an 18" RCP gate-operated low entrance inlet and a high stage weir. Discharge is through a 60" RCP which empties directly into the outlet channel. The top of the 5'x15' rectangular riser is open on all four sides and is capped with an anti-vortex slab 2 feet above the weir crest. A 100 foot wide

auxiliary spillway is located at the right abutment and has a negatively sloped entrance, a level control section, and a positively sloped outlet. A 6" perforated toe drain collector pipe extends across the downstream toe and discharges through the outlet headwall.

b. Location

Stony Brook Watershed Dam No. 3 is located in Hopewell Township, approximately two miles east of the center of the Borough of Pennington, Mercer County, New Jersey. The dam impounds an unnamed tributary of Stony Brook about 400 feet upstream of their confluence.

c. Size Classification

The maximum height of the dam is 28 feet and the maximum storage is estimated to be 463 acre-feet. Therefore, the dam is in the small size category as defined by the Recommended Guidelines for Safety Inspection of Dams (storage capacity less than 1,000 acre-feet).

d. Hazard Classification

No significant development lies downstream of the dam. The Rosedale Park playground facilities located at the dam site are situated near the left abutment where the failure potential is lowest. There are no downstream roads within several miles of the dam site and economic loss, except for the dam itself, would be minimal in the event of a failure. It is therefore recommended that this dam be classified in a low hazard category.

e. Ownership

The dam is owned by the Mercer County Park Commission, Mercer County Board of Chosen Freeholders, Trenton, New Jersey.

f. Purpose of Dam

The dual purpose of the dam is to provide flood/sediment retention on this tributary of Stony Brook and to enhance the recreational facilities for the surrounding County Park.

g. Design and Construction History

The dam was designed by the U.S. Soil Conservation Service and constructed in 1968-69. Detailed construction plans and design documents are available. It is unknown who actually accomplished the construction, but the dam appears to have been constructed in accordance with the design.

h. Normal Operating Procedures

The dam is maintained and operated as an integral part of Rosedale Park by personnel of the Mercer County Park Commission. See Section 4 for additional procedures.

1.3 PERTINENT DATA

a. Drainage Area

The drainage area is 1.5 square miles of rural, rolling countryside.

b. Discharge of Dam Site

Total spillway capacities at top of dam elevation - 7,900 cfs

c. Elevation (ft. above M.S.L.)

Top of dam - 158.4

Principal spillway crest - 151.5

Auxiliary spillway crest - 153.8

Upstream invert 18" Ø diversion pipe - 134.0

Riser floor & invert of 60" Ø pipe - 133.0

Streambed at centerline of dam - 132+

d. Reservoir

Length of maximum pool - 3,500 feet Length of recreation pool - 3,100 feet e. Storage (acre-feet)

Recreation pool (Principal spillway crest) - 182
Flood control pool (Auxiliary spillway crest) - 265
Top of dam - 463

f. Reservoir Surface (acres)

Top of dam - 56 Recreation pool - 30

g. Dam

Type - Earth with a drop inlet principal spillway and an earth channel auxiliary spillway

Length - 1,900 feet

Height - 28 feet

Top width - 15 feet

Side slopes - 25H:1V

Zoning - Two zoned

Impervious core - Compacted fine-grained material (95% max. density)

Cutoff - Variable depth, 10' wide impervious cutoff key monolithic with core.

h. Diversion and Regulating Tunnel

None

- i. Spillway
 - 1) Principal Spillway

Type - Drop inlet with 60" diameter RCP outlet (crest elevation - 151.5)

Gates - One 18" low level sluice gate (Inv. elevation 134.0)

2) Auxilliary Spillway

Type - trapezoidal channel at right abutment (crest elevation - 153.8)

Width of channel - 100 feet

U/S Channel - Negatively sloped, 380' long grassed inlet.

D/S Channel - Positively sloped, 320' long grassed outlet.

j. Regulating Outlets

Gate controlled, 18" \emptyset RC entry pipe (discharges onto floor of drop inlet).

SECTION 2 - ENGINEERING DATA

2.1 DESIGN

Complete details of the design plans, hydraulic determinations, and subsurface information were available at the Soil Conservation Service offices in Somerset. All design was done in accordance with SCS criteria and was discussed with their engineering personnel who explained the various design and operational features of the dam, particularly the hydraulic design parameters. Their geotechnical report concludes that the shale and silty gravel foundation materials present no stability problems and, according to their calculations, a factor of safety of 1.75 was concluded to be adequate. The closed conduit spillway geometry was determined by methods used in model studies at the St. Anthonys Falls Hydraulic Laboratory in Minneapolis. The concrete anti-vortex slab prevents the formation of a crotch and boil region (and the attendant reduction due to the entrance of air) in the inlet.

2.2 CONSTRUCTION

The construction appears to have closely followed the contract plans. There have been no major structural modifications.

2.3 OPERATION

As the principal purpose of the dam is to reduce urban flooding as well as to establish a recreational area, its operation appears to function properly under the aegis of the Park Commission.

2.4 EVALUATION

a. Availability

Sufficient engineering data was obtained to assess the structural stability with regard to the embankment zoning. The foundation stability was delineated in the various soils reports prepared by the SCS (which

analyzed all geotechnical aspects in considerable detail). The dam site lies in the Brunswick formation which consists of red silty shales and siltstone. The overburden ranges from 4' to 8' thick and consists of soft, silty, clayey alluvium, overlying roughly 2 feet of very firm, residual gravelly shale at the right abutment. The center section of the dam and left abutment are overlaid with 2 to 3 feet of alluvium over the compact gravel layers. The compacted core material was excavated from the right abutment area, while exposed bedrock at the left abutment was covered with a compacted soil layer to minimize seepage. The silty alluvium found at the site was utilized as embankment material, but the drain filter material was imported from off-site quarries.

b. Adequacy

The field inspection and review of the available design plans reveal that the dam is structurally sound and well-built. It is believed that the data available is adequate to render this assessment without recourse to gathering additional information.

c. Validity

The validity of the engineering data available is not challenged and is accepted without recourse to further investigations.

SECTION 3 - VISUAL INSPECTION

3.1 FINDINGS

a. General

Visual inspection was conducted on 8 December 1978. Weather conditions at the time of the inspection were overcast and cool. The overall appearance of the dam and appurtenant structures was satisfactory. Water level in the lake at the time of the inspection was at normal pool elevation 151.5 and the tailwater was at elevation 132.2. The region surrounding the site and immediately downstream is undeveloped, as is most of the upland drainage area.

b. Dam

In general, the dam appears to be in a stable condition. A substantial grass cover protects the slopes of the main embankment and the auxiliary spillway. The crest has vehicular tracks along its entire length despite the existence of a transverse wooden barrier. Deeper rutting was also noted on the approach section of the auxiliary spillway. The ruts were 4 to 5 inches deep and filled with water, which may be indicative of a high water table at this location. A seven foot long vertical surface crack was noted about halfway up the backslope of the embankment near the right end of the dam. The one inch wide by six inch deep crack exhibited some sloughing at the upslope end and appeared to have resulted from a combination of seepage, frost-action and surface erosion. Additional minor erosion was noted on the embankment near the left abutment. At this location the grass cover has been torn up by equestians riding on the embankment slopes. In general, the observed percolation appears to be the result of a high natural water table and is not of a concentrated nature in any location. It is not a result of piping or seepage through the engineered embankment.

c. Appurtenant Structures

The concrete drop inlet and anti-vortex slab are located only a few feet offshore which permitted a close examination. While the 18" sluice gate stem wheel is missing, the remainder of the structure is in good condi-The concrete has a fresh appearance and no structural cracking was noted. Similarly, the outlet conduit and headwall are in satisfactory condition with only some minor efflorescence noted on the headwall. The right toe drain discharge pipe was dry, while the left drain was flowing freely. The grass-covered auxiliary spillway is approximately 100 feet wide and is in good condition with the exception of the previously described vehicle tracks. There is a pile of earth deposited near the right wall of the channel which apparently will be used for maintenance this spring.

d. Reservoir

The lake created by Stony Brook Dam No. 3 is part of the Mercer County Park system and is bounded on all sides by park property. The reservoir is surrounded by gently sloping, open to lightly wooded terrain and the shoreline is fairly well developed. The lake is clear of debris.

e. Downstream Channel

The area below the dam is undeveloped for as far as the next flood control structure which is located 1.5 miles downstream. The narrow discharge channel immediately below the dam has been excavated from the shale bedrock and has gently sloping banks which are devoid of vegetation for roughly 100 feet downstream. The area below the left abutment is developed into a small playground with an adjoining comfort station. A sanitary leaching field for a comfort station is presently being excavated about 185 feet downstream.

This excavation is about 5 feet deep. Upon its backfilling and completion, the inspection team felt this will have no effect upon the dam stability.

SECTION 4 - OPERATIONAL PROCEDURES

4.1 PROCEDURES

Stony Brook Dam No. 3 is part of a 580 acre passive recreational area under the jurisdiction of the Mercer County Park Commission. As such, the dam is routinely maintained and patrolled by Park Department personnel. Maintenance is generally limited to grounds keeping. There are no documented operational procedures which apply to the dam gate or sstructure.

4.2 MAINTENANCE OF DAM

Maintenance personnel of the Park Commission are on duty in the area on a daily basis. Routine maintenance of the dam includes mowing, debris removal and minor repairs when required. This includes removal of debris in or around the drop inlet and discharge channel as well as repair of eroded surfaces.

4.3 MAINTENANCE OF OPERATING FACILITIES

The only regulating feature at this dam is the gate-controlled, low level, 18" emergency drain pipe. The gate has never been opened and there are no operating instructions available. In addition, the stem wheel is presently stored at the office of the utility engineer (some 5 miles from the dam). The dam is formally inspected once a year by personnel of the Soil Conservation Service and Park Commission. Minor remedial action prescribed by the inspection team is performed by the MCPC maintenance crews while major repairs, when required, are referred to the SCS.

4.4 DESCRIPTION OF ANY WARNING SYSTEM IN EFFECT

There is no warning system in effect although MCPC personnel monitor the dam during heavy storms.

4.5 EVALUATION OF OPERATIONAL ADEQUACY

While the purpose and function of this dam requires little in the way of operational procedures, it is felt that some additional training of park maintenance and patrol personnel could improve the operational efficiency and safety of the dam. The stem wheel should be stored at the dam site and maintenance personnel and park police should be instructed in visual indications of dam deterioration and steps to remedy specific defects.

SECTION 5 - HYDRAULIC/HYDROLOGIC

5.1 EVALUATION OF FEATURES

a. Design Data

Based on the criteria in the Recommended Guidelines for Safety Inspection of Dams, the 100-year frequency event was selected as the design storm by the inspecting engineer. Precipitation data was obtained from Technical Paper 40 and NOAA Tech. Memo NWS - Hydro #35. Storage data and time of concentration were obtained from the Soil Conservation Service design calculations and reviewed in the context of current inspection criteria. Inflow to the reservoir for the selected 100-year storm was computed utilizing the HEC-1 computer program which yielded a peak inflow of 2,152 cfs. Routing this through the controlled-release reservoir reduced the discharge to 1,563 cfs. The combined spillways have a maximum discharge capacity of approximately 7,900 cfs before overtopping occurs and can therefore accommodate the design flood. The depth of crest flow in the auxiliary spillway is less than 1.5 feet for this design discharge.

b. Experience Data

The dam was originally designed for a 100-year frequency storm using a time of concentration of 1.5 hours. The auxiliary spillway height was established so that the design flow depth (according to SCS procedures), leaves slightly more than 2 feet of freeboard to the dam crest. In the original design, the detailed hydraulic analyses (including infiltration studies), were exhaustively performed by the SCS to quantify final design values against the economical apportionment of the dam.

c. Visual Observations

With the water at normal pool elevation at the time of inspection, approximately 2 cfs was flowing out of the 60" outfall. According to park personnel, no flow has ever been transmitted over the auxiliary spillway. Visual observations confirmed all the aspects and assumptions of the original hydraulic design.

d. Overtopping Potential

There are no records of the dam having been overtopped and the main and auxiliary spill-ways can easily accommodate the design flood.

e. Drawdown Potential

Drawdown capability is provided by the 18" operable sluice gate. Assuming no tailwater, it would take approximately 3 days to dewater the lake from normal pool elevation.

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SECTION 6 - STRUCTURAL STABILITY

6.1 EVALUATION OF STRUCTURAL STABILITY

a. Visual Observations

In view of the relative age of the dam embankment, the well-designed and supervised construction, and the continuous maintenance, the dam at
Stony Brook Site No. 3 is deemed to be in a
good to excellent condition. The main embankment crest and adjoining cut slopes along the
auxiliary spillway are at true design grade.
The toe drain left of the spillway outfall
appears to be under a continuous but modest
head due to seepage and/or percolation. In
summary, nothing was visually noted to create
or worsen present conditions that cannot be
readily maintained or corrected.

b. Design and Construction Data

From the review of the SCS soils report, hydraulic recommendations and contract plans for the initial construction, the design appears to be well-engineered, reflects a conservative approach and employs conventional analytical techniques. In view of the condition of the dam and hazard classification, it is believed that additional studies are unnecessary under the purview of PL 92-367.

c. Operating Records

The performance of this structure has been satisfactory since its completion. However there are no formal operating records available.

d. Post Construction Changes

There have been no major modifications since the initial construction that affect the overall structural integrity of the dam.

e. Seismic Stability

The dam is located in Zone 1 and has negligible potential vulnerability to seismic loadings.

Dams in this zone which have an adequate factor of safety under static loading conditions will also prove stable under dynamic loading conditions.

SECTION 7 - ASSESSMENTS/RECOMMENDATIONS/ REMEDIAL ACTIONS

7.1 DAM ASSESSMENT

a. Safety

Subject to the inherent limitations of the Phase I visual inspection, Stony Brook Dam No. 3 is judged to be in a good to excellent overall structural condition. Overtopping of the dam is a very remote possibility and no seriously detrimental conditions were observed. The dam is recommended to be placed in a low hazard category due to location within the officially designated Mercer County Parklands. The combined spillway capacities considerably exceeds the selected 100-year frequency design flood.

b. Adequacy of Information

The information made available by the Soil Conservation Service is deemed to be adequate regarding the analyses and evaluation of safe operation and structural stability.

c. Urgency

No urgency is attached to implementing the remedial measures set forth below.

d. Necessity for Further Study

In view of the overall condition of this dam and the fact that it is continually monitored by trained personnel, additional inspections under the purview of P.L. 92-367 are deemed to be unnecessary. The County Parks Department in conjunction with SCS engineers, maintain a system of annual inspections which basically reflect the requirements mandated under P.L. 92-367.

7.2 RECOMMENDATIONS/REMEDIAL MEASURES

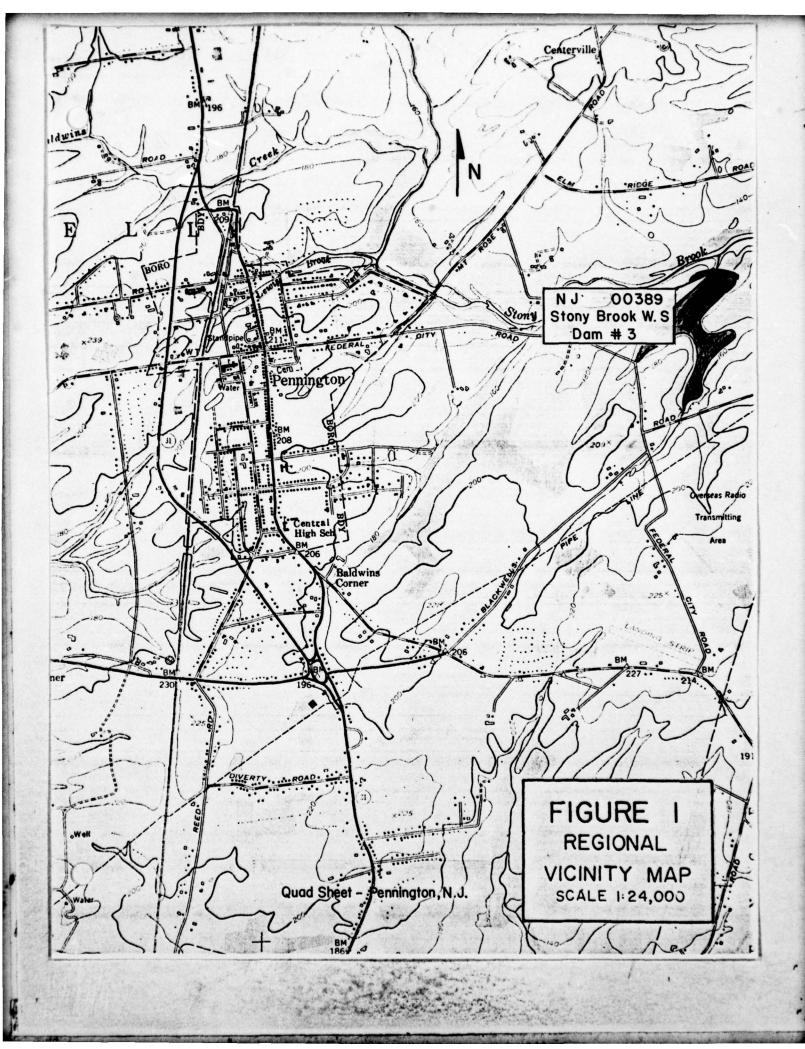
a. Recommendations

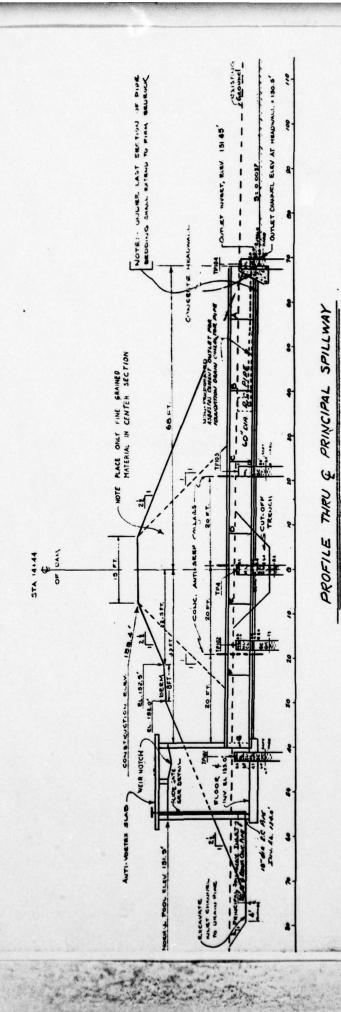
Under the present maintenance program, it is recommended that the following be taken under advisement in the future:

- Regrade the eroded backslopes and sides and reseed the barren areas.
- Continue to monitor the backslope seepage and the subgrade drains.

b. O&M Maintenance and Procedures

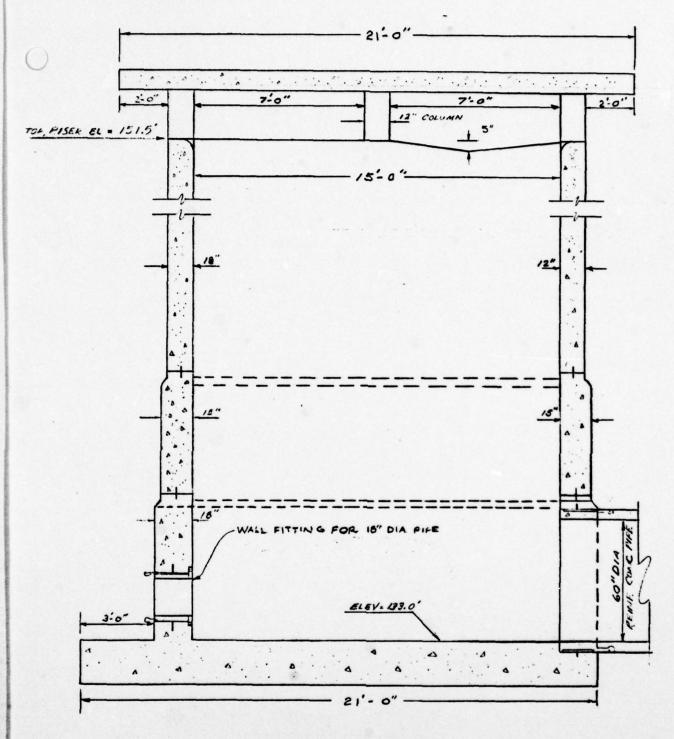
In view of the assessment contained herein, no additional procedures other than those presently in effect appear to be required. However, it is recommended that additional training be considered for park personnel relative to maintenance and inspection.





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Figure 2



SECTION ON F

DETAIL - CONCRETE RISER

FIGURE 4

Check List Visual Inspection Phase 1

New Jersey Coordinators NJDEP	Temperature 45	Tailwater at Time of Inspection 132± K.S.L.				Recorder
County Mercer State	Weather Cloudy Tempe	Inspection 151.5 M.S.L. Tailw	K. Jolls			C. Chlut
Name Dam Stony Brook W.S.No.3 County	Date(s) Inspection 12/8/78	Pool Elevation at Time of Inspec	Inspection Personnel: T. Chapter	c. Chlut	E. Simone	

8	9	
	ENDAPTOIENT	
VISUAL EXACTINATION OF	OBSERVATIONS	REMAKS OR RECOMMENDATIONS
SURFACE CRACKS	Shallow vertical cracks on right embankment.	Cracks appear to be the result of frost action and surface erosion rather than a structural deficiency. (See photo).
UNUSUAL ROVERENT OR CRACKING AT OR BEYOND THE TOE	None observed.	
SLOUGHING OR EROSION OF ENEANGENT AND ABUTHERT SLOPES	Tire ruts on crest of dam. Minor erosion at headwall of outlet. Hoof prints on and around embankment.	Barrier across crest. The tracks on slope of embankment at location of barrier.
VERTICAL AND HORIZONTAL ALINEMENT OF THE CREST	Satisfactory alignment. No signs of differential settlement noted.	

RIPRAP FAILURES

N/A

00		
	EMBANGENT	Sheet 2
VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
	An excavation for septic system at recreational facilities was opened 185 feet below the left embankment.	Excavation filled with ground water probably coming from lake. Excavation should be backfilled and septic system relocated. (See photo).
JUNCTION OF ENBANDENT AND ABUTHENT, SPILLMAY AND DAN	Left embankment grades into natural terrain. Right embankment abuts the auxiliary spillway. Both satisfactory.	
ANY NOTICEABLE SEEPAGE	Light seepage along toe of central portion of embankment and over the headwall of the outlet structure.	Flows are widely dispersed and none are concentrated. (See photo).
STAFF CAGE AND RECORDER	None	

Left drain flowing freely. No discharge from right drain. (See photo). 2-6" ϕ toe drains - one on each side of the outlet pipe in good condition.

DRAINS

	REMARKS OR RECONSISHDATIONS	See photo	See photo	See photo	See photo	
OUTLET WORKS	OBSERVATIONS	Outlet conduit and headwall in new condition. No deterioration noted.	Concrete in new condition. No deterioration noted. Wheel for gate steam missing.	No deterioration noted.	Narrow, shallow sloping sides are defoliated for 100' below outlet.	At elevation 134 M.S.L. of intake structure. Not visible to inspection team.
	VISUAL EXAMINATION OF	CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT	INTAKE STRUCTURE	OUTLET STRUCTURE	OUTLET CHANNEL	EMERGENCY GATE

	REMARKS OR RECOMMENDATIONS						
UNGATED SPILLWAY	OBSERVATIONS	Principal spillway: 60" & drop inlet pipe in good condition.	Auxiliary spillway: Good condition.	Principal spillway: None Auxiliary spillway: Good condition. 300' of grass covered entrance channel.	Principal spillway: Good. Auxiliary spillway: Good. 350' of outlet channel, thickly grassed.	None	
C.	VISUAL EXAMINATION OF	CONCRETE WEIR		APPROACH CHANNEL	DISCHARGE CHANNEL	BRIDGE AND PIERS	

To the second

	REMARKS OR RECOMMENDATIONS							Believed to be stored at office of utility engineer at Mercer County Airport - approximately 5 miles away.
GATED SPILLWAY	OBSERVATIONS	N/A		N/A		N/A	N/A	Control wheel for gate stem is missing.
	VISUAL EXAMINATION OF	CONCRETE SILL		APPROACH CHANNEL		DISCHARGE CHANNEL	BRIDGE AND PIERS	CATES AND OPERATION EQUIPMENT

Take !

VISUAL EXAMINATION	INSTRUMENTALION OBSERVATIONS	REMARKS OR RECONSENDATIONS
MONUMENTATION/SURVEYS	Square cut bench mark at downstream end of Federal City Road Bridge. TBM in power pole at bend in Farm Lane.	
OBSERVATION WELLS	None	
WEIRS	"V"-notch weir in one section of drop inlet, but not utilized for flow determination.	
PIEZOGETERS	None	
отнея	None	

RESERVOIR

Desiltation is one of the dam's primary functions. REMARKS OR KECOMMENDATIONS Gently sloping on all sides. Light treed to southwest. Heavier foliage to east and southeast. OBSERVATIONS None VISUAL EXAMINATION OF SEDIMENTATION SLOPES

(

DOWNSTREAM CHANNEL

VISUAL EXAMINATION OF	=	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONDITION (CESTRUCTIONS,	Principal spillway:	Good although denuded of vegetation.	Channel clear of debris.
DEBKID, ELC.)	Auxiliary spillway:	Outlet channel in good condition - damp surface.	
SLOPES	Principal spillway:	Principal spillway: 1.5H: IV side slopes cut into outcropping shale.	
	Auxiliary spillway:	3H: 1V side slopes in good condition.	
APPROX BATE NO. OF HONES AND POPULATION	No downstream constr	No downstream construction or developments.	Construction of playground underway near dam.

Ground at construction site approx. El. 150+.

ENGINEERING DATA CHECK LIST

DESIGN, CONSTRUCTION, OPERATION

T.

TIAN OF UNI

Available from U.S. Department of Agriculture Soil Conservation Service 1370 Hamilton Street, Somerset.

REGIONAL VICINITY MAP

Available

CONSTRUCTION RESTORY

Available from Soil Conversation Service

TYPICAL SECTIONS OF DAR

Available from Soil Conservation Service

Available from Soil Conservation Service

HYPROLUGIC/HYPRAULIC DATA

CUTLETS - PLAN

-CONSTRAINTS -DISCIMPGE PATTERS - DELVIES

Available from Soil Conversation Service

Available from Soil Conservation Service Available from Soil Conservation Service Available from Soil Conservation Service

Not Kept

RAINFALL/IGSTRVOIR RECORDS

Available from Soil Conservation Service. REMARKS DESIGN REPORTS

Available from Soil Conservation Service

GROLOGY REPORTS

DESIGN COMPUTATIONS
HYDROLOGY & HYDRAULICS
DAM STABILITY
SEELAGE STUDIES

Available from Soil Conservation Service Available from Soil Conservation Service Available from Soil Conservation Service Available from Soil Conservation Service

NAVERLES DEVESTIGATIONS BORING RECORDS LABORATORY FIELD

Available from Soil Conservation Service Available from Soil Conservation Service Available from Soil Conservation Service Available from Soil Conservation Service

POST-COMSTRUCTION SURVEYS OF DAM

None performed

BORROW SOURCES.

Available from Soil Conservation Service

REMARKS None MONITORING SYSTEMS

1

MODIFICATIONS

HIGH POOL RECORDS

None

None kept

POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS

None performed with exception of annual inspection reports which are available from SCS.

PRIOR ACCIDENTS OR FALTURE OF DAM DESCRIPTION PERONTS

None

MALETETANCE OPERATION RECORDS

None kept

REMAIRES

SECTIONS Available from Soil Conservation Service

SPILLINY PIAN

16

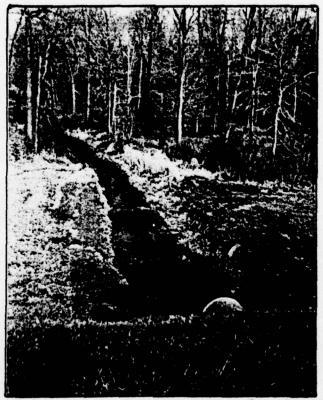
Available from U.S. Department of Agriculture Soil Conservation Service

DFTAILS Available from Soil Conservation Service

OPERATING EQUIPMENT Available from Soil Conservation Service FIAIS & DETAILS

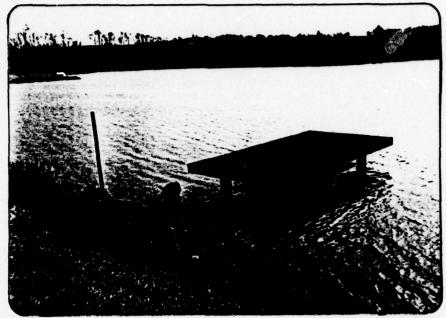


Looking East



December, 1978

View downstream

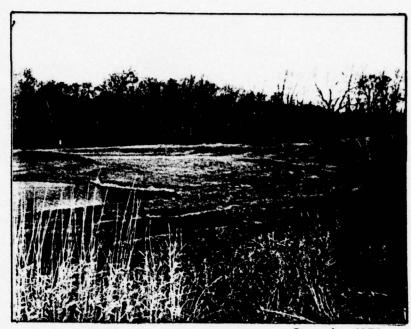


December, 1978

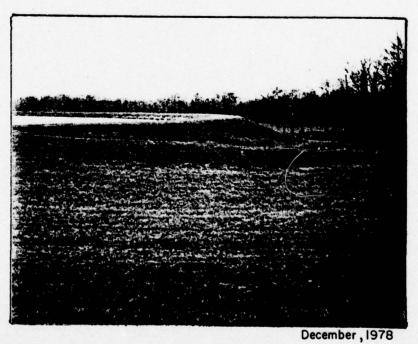
View of intake structure



View of outlet structure



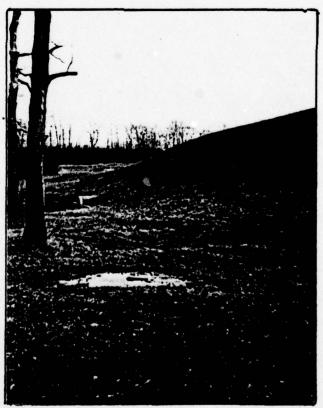
December, 1978 View of auxiliary spillway



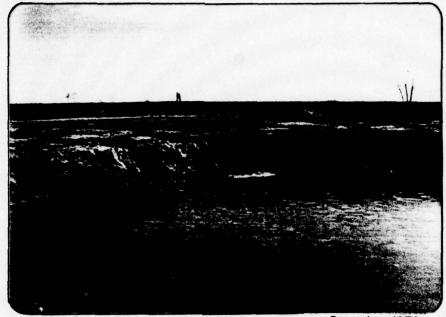
View of auxiliary spillway



Seepage at toe



December, 1978
Seepage at toe of left embankment



December, 1978

View towards dam

SITE OF PROPOSED LEACHING FIELD

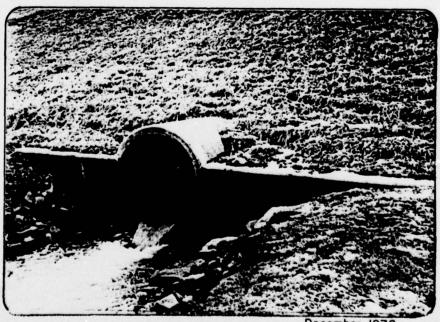


View downstream

December, 1978



Vertical surface cracks



December, 1978
Toe drains and seepage at outlet structure

CHECK LIST HYDROLOGIC AND HYDRAULIC DATA ENGINEERING PATA

DRAINAGE AREA CHARACTERISTICS: 1.5 sq.mi.
ELEVATION TOP NORMAL POOL (STORAGE CAPACITY): Elev. 151.5 (182 acre-feet)
ELEVATION TOP FLOOD COMERCE POOL (STORAGE CAPACITY): 153.8 (265 acre-feet)
RLEVATION MAXIM DESIGN POOL: Elev. 154.4
ELEVATION TOP DAM: Elev. 158.4
CREST:
nt 152 0 M C T (Anniliant millions amak)
b. Type Vegetated auxiliary spillway channel c. Width 100 feet
c. Width 100 feet
d. Length 380' entrance; 30' control section; 320' outlet
e. Location Spillover Right abutment
f. Number and Type of Gates None
OUTLET WORKS:
a. Type 2 stage drop inlet with 60" Ø R.C. discharge pipe
b. Location Station 14+44 c. Entrance inverts Weir at 151.5 M.S.L.; 60" ø at 133.0 M.S.L.
c. Entrance inverts Weir at 151.5 M.S.L.; 60" ø at 133.0 M.S.L.
d. Exit inverts 130.5 M.S.L. e. Emergency draindown facilities 18" Ø R.C.P. at elevation 134.0 M.S.L
e. Emergency draindown facilities 18" p R.C.P. at elevation 134.0 M.S.L.
Who agreement of colors andre. None
SYDROPETEUROLOGICAL GAGES: None
a. Type
c. Records
C. IV. GLUD
MAXIMUM NON-RAMAGING DISCHARGE. 7900 cfs

D.YE	J.M.	DATE	2-79
		_	

LOUIS BERGER & ASSOCIATES INC.

SHEET NO. AL OF

CHRD. BY.____DATE.

STONY BROOK W.S. 3 DAM INSPECTION

SUBJECT

Time of concentration as computed by s.c.s.

Description of course	Slope of	Length (1)	Velocity of	time (sec)	
of runoff water	course	of course	runoff water		
	(%)	(ft)	(v) (ft/sec)	= (3) + (4)	
 REACH I - overland	< 3	2200	0.8	2750	
REACH I - Chonnel	0.5	1400	1.8	7 78	
REACH I - Channel	0.5	1300	1.7	765	7
REACH D - channel	0.5	1900	2.4	792	
REACH I - channel	1.2	1400	2.6	538	
			Sum	5623	

$$T_c = \frac{1}{\sqrt{x3600}} = 1.56 \text{ hours} \quad \text{Use } 1.5 \text{ hours}$$

use 0.25 hr interval

$$T_p = \frac{0.25}{2} + 0.6 T_e = 1.03 \text{ hrs.}$$

Drainage area = 1.5 sq miles

$$\therefore Q_{p} = \frac{484 \times 1.5 \times 1}{1.03}$$

= 708 cfs

SCHARE PRESS

BY. D. J. M. DATE 2-79 CHKD. BY DATE

LOUIS BERGER & ASSOCIATES INC.

STONY BROOK W.S. 3 DAM INSPIECTION

SHEET NO. A2 OF PROJECT C227

SUBJECT

T	THO	Dimension less Ordinate	Q	
hrs		(DO) = Q/Qp	= DoxQp	
0.25	0.24		7.	
0.50	0.49	0.10	71	
		0.41	290	
0.75	0.73	0.81	573	
1.00	0.97	0.99	701	
1.25	1.21	0.91	644	
1.50	1.46	0.69	489	
1.75	1.70	0.49	347	
2.00	1.94	0.35	248	
2.25	2.18	0.24	170	
2.50	2.43	0.17	120	
2.75	2.67	0.11	78	
3.00	2.91	0.08	57	
3.25	3.16	0.06	42	
3.50	3.40	0.043	30	
3.75	3.64	0.031	22	
4.00	3.88	0.018	13	
4.25	4.13	0.015	11	
4.50	4.37	0.011	8	
			£ 3914	

Check unitgraph

 $\frac{3914 \times 12 \times 3600}{4 \times 1.5 \times 5280^2} = 1.0108$ = 1 inch over the area so 0.K.

KAUR PRESS

BY DJM. DATE 1-79

LOUIS BERGER & ASSOCIATES INC.

SHEET NO. A3 OF.

CHKD. BY____DATE____

PRECIPITATION DATA FROM T.P. 40 (See depth duration curve overleaf) 8 NOAA Technical memorandum NWS HYDRO-35

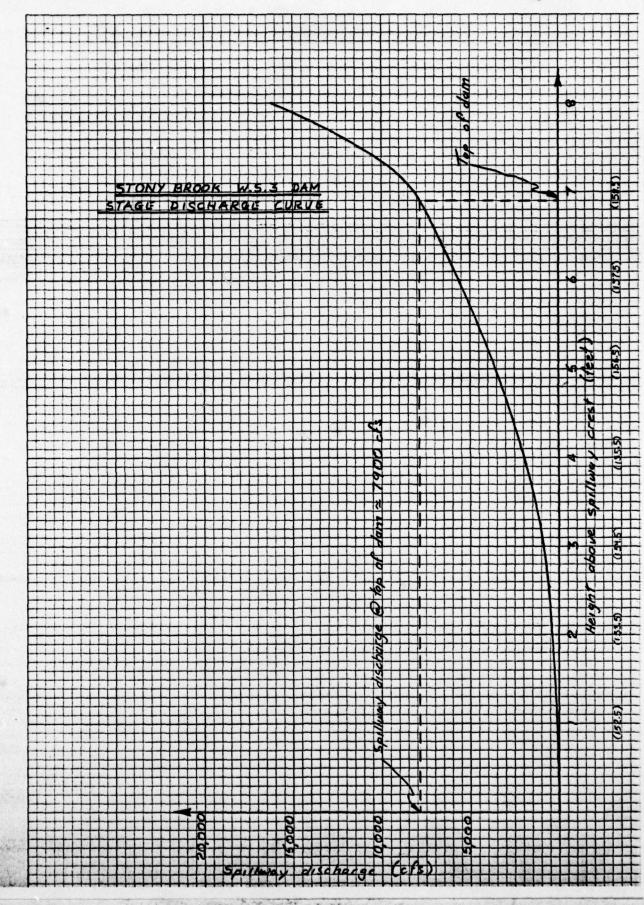
Time	Precipitation	Δ	Rearrange A
0.25	1.7	1.7	0.06
0.50	2.4	0.7	0.06
0.75	2.8	0.4	0.06
1.00	3.1	0.3_	0.06.
1. 25.	3.5	0.4	0.07
1.50	3.7	0. 2	0.07
1.75	3.86	0.16	0.08
2.00	4.00	0. 14	0.02
2 25	4 11	0.11	0.09
2.50	4.22	0.11	0.09
2. 75	4.31	. 0.09	. 0.11
3.00	4 40	0 09	0.11
3.25	4.49	0.09	0.30
3 50	4.57	30.0	0.70
3.75	4.64	0.07	1.70
4.00	4.71	0.07	0.40
4.25	4.78	0.07	0.40
4.50	4.84	0.06	0.20
4.75	4.90	0.06	0.16
5 00	4.96	0.06	0.14_
5.25	5.02	0 06	0.07
5.50	5.08	0.06	0.06
5.75	5:14	0.06	0.06
6.00	5.20	0.06.	0.06

BY D. J. M DATE 1-79 SUBJECT T. P. 40 & NWS HYDRO-35 SHEET NO. A4 OF DEPTH DURATION CURUE JOB NO. C227 STONY BROOK W. S. 3 DAM INSPECTION inches of rainfall

CHKD. BY.____DATE____

LOUIS BERGER & ASSOCIATES INC. SHEET NO. A5 OF STONY REDOK W.S. 3 DAM INSPECTION PROJECT. C.22.1

	flow	over	riser.	Through	60"	Auxili	lary	
we	ir flow		ert flow			Spille		
	38'							
	0 0		Q	H	a	H	·Q	
	3.1 11			16.5	471			
2	3.1 33	3		17.5	485			
		3	581	18.5	499	0.7	325	
		4	670	19.5	512	1.7	1408	
		5	750	20.5	525	2.7	3005	
		6	821	21.5	538	3.7	5017	
		7	887	22.5	550	4.7	7383	
		8	948	235	562	5.7	10060	
		10						
0	er Dam			£ Q	flow	, throu	gh ouxillar	y
	= 1800						ing manning	
4	c	Q	H	Q			= 0.05	
			/	118	assu	me rect	angular chai	nnel
			2	333		wide		
			3	824				
			4	1,920				
			5	3,530				
	i de la composition della comp		6	5,555				
0.1	2.7	154	7	8,087				
1.1	2.7	5607	8	16,229				
	45-10-3090							
fo	- flow t	hrough	60" pipe	tailwater	Elev. o	P +136	assumed	
		ula use	1.					
	4,011	T. Holys	Q		100	H		11 11 11 11 11
eson s				2.5	204(1+	(e) + 46	06.18 n2 L	
					D4		D'4/3	



46 0706

KOE 10 X 10 TO THE INCH - 7 X 10 INCHES

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BY D.J.M. DATE 2-79

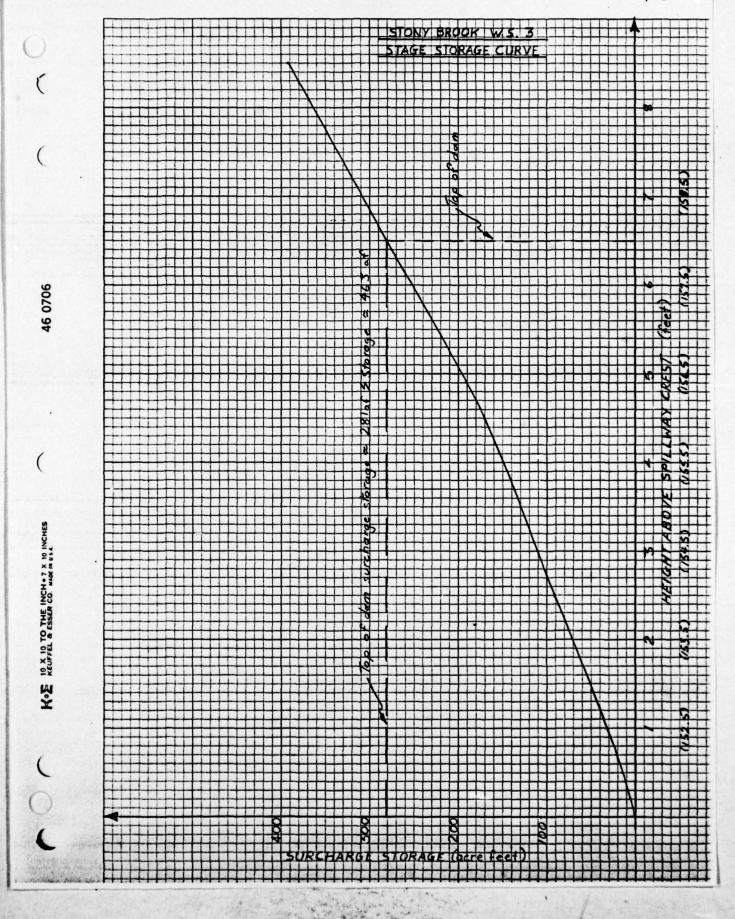
LOUIS BERGER & ASSOCIATES INC.

SHEET NO. A7 OF PROJECT 6 227

STONY BROOK W. S. 3 DAM INSPECTION

Stage storage data as calculated by Soil Conservation Service

Elevation (feet)	Storage (acre feet)	Surcharge Storage (acre feet)		
151.5	182	0		
152.0	197	15		
154.0	274	92		
156.0	35.2	170		
158.0	463	281		
160.0	574	392		



	SURCHARGE STORA		
ABOVE CREST		data for	
ABOVE CREST		gara tor	
CREST	CUP-ULDA II		program
CREST	CUP-ULPA II		
CREST	CIDAULDA F OT O		
CREST	CUPA UL DA F CT. C.		
CREST	SULCHARUTE STOKE	G-E	SPILLWAY DISCHAM
A STATE OF THE STA	(acre feet)		(cfs)
	0		0
	32		. 118
	70		333
	110		824
	150		1920
	196		3,530
	252		5,655
	281		7,200
	309		9,651
	364		19,550
	41111111		
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BY LB	DATE	FFR'7	9
5T	DAIL		.4

LOUIS BERGER & ASSOCIATES INC.

SHEET NO. ALO OF.

STONY BROOK SITE #3

SUBJECT DRAWDOWN COMPUTATIONS

Assuming no inflow into the reservoir and no tailwater.

ELEV.	STORAGE ACRE-FT	DIFFERENTIAL	DISCH ACTUAL CFS	AVER.	AVERAGE DISCHARGE RAE-FT/DAY	DRAWDOWN	
	ACKE-F1	ACRE-FT	CFZ	CFS	HUKE-FIJDAY	DAYS	+
151.5	182		43.1				+
151.7	102	42		42.2	83.7	.5	1
150	140		41.2				
		45		39.8	78,9	.6	
148	95		38.4				-
		30		36.9	73.2	.4	1
146	65		35.4	- 50 ut-15	1 7 7 7		1
		25		33.8	67	4	 -
144	40		32.1				-
		10	40 11	30.7	60.1	.2	4
142	30		28.4	26.3	52.2	.2	-
140	20	10	24.2	26.7	JL.L	- 12	-
170	20	16	24.6	21.6	42.8	.2	1
138	10		19.0				
		5		15.4	30.5	.2	
136	5		11.8				
		5		5.9	11.7	,4	
134.75	0		0				
			10				-
							1

Q=AV 29H Klosses	KLOSSES = KENTRANCE + KERIT + K	friction
= π (.75) ^ε √ 64.41	=.5+1+ 29:(0)9(1)	n= 0.012
• 10.54 H ^V	= 1.5+ 29.1(.012)=(20)	L= 2011

	IMDAT					ASSOCIATES		SHEET NO.	
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SUBJEC									
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*****	STONY BR	US 3 DOK DAM INSI ULLIGAN	PECTION	NORTH GR	OUP C227				
Charles	FERRUARY	1979					Core secondocara	nations programs	
H	T. E. S.	NG NHR	NMIN I	JOB SPEC	R IMIN	METRC IPLT	IPRT NSTA	N	
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				UNIT GR					
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78.	57. UNI	42.	TALS 3	914. CFS	OR 1.01	13 11 INCHES OVER	THE AREA	•	
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				END-OF-P					
			TIME 1	0.06	0.00	0.			
			2	0.06	0.00	0.			
			4	0.06	0.00	0.			
		Try	6	0.07	0.00	0.		To Company	*
			7	0.08	0.00	0. 3.			
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LOUIS BERGER & ASSOCIATES INC. BY DIM DATE SHEET NO. AJZ OF. STONY BROOK W.S. 3 CHKD. BY____DATE____ PROJECT_C-227 SUBJECT 10 0.09 0.06 0.11 11 0.08 87. 0.11 0.08 137. 0.30 0.27 198. 0.70 0.67 322. 1.70 1.67 650. 16 0.40 0.37 1233. 17 0.40 0.37 1848. 0.20 2152. 18 0.18 0.16 2093. 0.13 0.14 20 0.11 1608. 21 0.07 0.05 1481. 22 0.06 0.04 1182. 23 0.06 0.04 914. 0.06 0.04 700. 25 0.0 0.0 526. 26 0.0 403. 0.0 27 0.0 0.0 302. 28 0.0 220. 0.0 29 0.0 0.0 156. 107. 30 0.0 0.0 0.0 31 0.0 .51 . 32 0.0 0.0 33 0.0 0.0 27. 34 0.0 0.0 35 0.0 10. 36 0.0 6. C.0 0.0 0.0 38 2. 0.0 0.0 39 0.0 1. 0.0 40 0.0 0.0 1. 41 0. 0.0 0.0 42 0.0 0.0 0. 43 0.0 0.0 0. 44 0.0 0.0 9 . 45 0.0 0.0 0. 0.0 0.0 0. 47 0.0 0.0 0. 48 0.0 0.0 0. 0.0 0.0 50 0.0 0.0 0. 51 0.0 0.0 52 0.0 0. 0.0 53 0.0 0.0 0. 54 3 0.0 0.0 0. 55 0.0 0.0 0. 56 0.0 0.0 0. 57 0.0 0.0 0.0 0.0 0.0 0. 0.0 60 0.0 0.0 0. 61 0.0 0.0 0. 62 0. 0.0 0.7 63 0. 0.0 0.0 64 0.0 0. 0.0 65 0.0 0.0 0. 50 0.0 6.7 0.0 0.0 0. 66 0.0 0.0 69 0.0 0.0

HKD. BY	DATE DATE			STONY BROOK W.S. #3 PROJECT								
			TONY B	ROOK	STONY BROOK W. S. #3 PROJECT							
UBJECT												
the free body back								- indes				
				1 0.0								
				2 0.0	0.0	0.						
				3 0.0	0.0	0.						
				5 0.0	0.0	0.						
				6 0.0	0.0	0.						
				7 0.0	0.0	0.						
				9 0.0	0.0	0.						
			8	0.0	0.0	0.						
				0.0	0.0	0.	1-12					
	Total Control			3 0.0	0.0	0.						
			8	0.0	0.0	0.						
				5 0.0	0.0	0.						
			8	37 0.0	0.0	0.						
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		CFS	PEAK 2152.	6-HOUR 697.	24-HOUR 175.	72-HOUR 1	OTAL VOLUME 16776.	7				
		INCHES	2132.	4.32	4.33	4.33	4.33					
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		AC-FT		346.	341.	The second secon						
2.80		AC-FI		346.	347.							

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	*****	****						••••				
••••	*****	****	RESERVOIR	+++	**********	ING		****				
••••	*****	****	RESERVOTE 1 CUMP	HYCROGI 1ECUN 0	RAPH ROUT	JPLT JPF		••••				
••••	*****	G THROUGH F	RESERVOTR 1 CUMP	HYDROGI IECUN O ROU	RAPH ROUT	JPLT JPF	T INAME 0 1	••••				
••••	*****	G THROUGH F	RESERVOTE 1 CUMP	HYCROGI 1ECUN 0	RAPH ROUT	JPLT JPF 0	Y INAME 0 1	••••				
••••	*****	IG THROUGH ISTAL	RESERVOTR 1 CUMP 1 DLOSS 0.0	HYCROGI IECUN O ROU' CLOSS 0.0	TTAPE TING DATA AVG 0.6	JPLY JPF 0 JRES ISAN	Y INAME 0 1 E	****				
	*****	IG THROUGH ISTAL	RESERVOTR 1 CUMP 1 DLOSS 0.0	HYCKOGI IECUN O ROU CLOSS	TYAPE OTING DATA AVG 0.C	JPLT JPF 0	T INAME 0 1 E 0 K STORA	••••				
STOPAGE=	ROUTIN	G THROUGH FISTAGE 115	RESERVOTR 1 CUMP 5 1 0LCSS 0.0 8 NSTOL	HYDROGI IECUN 0 ROU: CLOSS 0.0 LAG 0	TYAPE OTING DATA AVG 0.G AMSKK 0.0	JPLY JPF 0 IRES ISAN 1 TS 0.0 0.0	T INAME 0 1 1E 0 1K STORA 0. 252. 281	-				
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